

**DEVELOPING ONE-OF-A-KIND COMPOSITE
STRUCTURES
FOR SCIENCE AND EXPLORATION AT
NASA'S GODDARD SPACE FLIGHT CENTER**

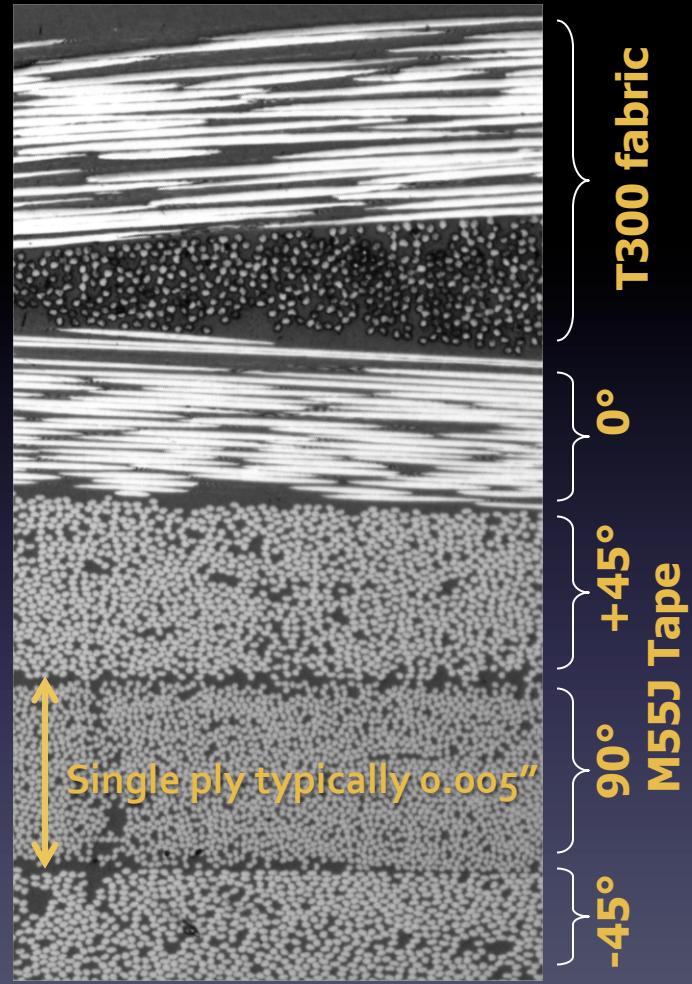
**Daniel L. Polis
NASA's Goddard Space Flight Center
December, 14 2011**

Outline

- Recent examples of composite structures designed and built by NASA and its partners
- Primary benefits of composites (carbon fiber reinforced plastics, CFRP's) for space structures
- New composite technology thrust areas at Goddard Space Flight Center (GSFC)

Common CFRP's for Space Applications

- Materials supplied as fiber pre-impregnated with resin, "prepreg", with fiber volume ~60% for tape and ~57% for fabric
- Unidirectional tape:
 - M55J fiber:
 - industry standard, good combination of stiffness and strength
 - Cyanate ester resin
 - 954-3 or RS-3
 - 350°F cure
 - low moisture absorption(~10% of epoxy)
- Biaxial fabric:
 - T300 fiber/cyanate ester resin
 - industry standard, high tensile and shear strength
 - plain weave fabric for simplicity and cost
- Two primary layups used:
 - Quasi-isotropic (QI) for omnidirectional loading and low distortion, e.g. $[0/45/90/-45]_s$
 - Biased layup for unidirectional loading and low distortion, e.g. $[0_3/45/0_2/-45]_s$



Quasi-isotropic tape w/
fabric outer plies

Recently Developed Composite Structures

Program	HST's Super Lightweight Interchangeable Carrier (SLIC)	JWST's Integrated Science Instrument Module (ISIM)	NESC's Composite Crew Module (CCM)
Configuration			
Type	Protoflight	Protoflight	Prototype
Flight	STS-125	Ariane V	Designed for Ares I
Composite benefit	Specific Stiffness	Thermal Distortion	Optimized load paths and biaxial tensile strength
Technology highlights	<ul style="list-style-type: none"> • Titanium metal matrix/integral end fitting struts • Human-rated primary structure 	<ul style="list-style-type: none"> • Cryogenic joinery • Hybrid laminates for "zero" CTE at cryogenic temperature 	<ul style="list-style-type: none"> • OOA 3D woven pi-preforms • OOA splice joint • Membrane loaded pressure dome

PRIMARY BENEFITS OF COMPOSITE FOR SPACE APPLICATIONS

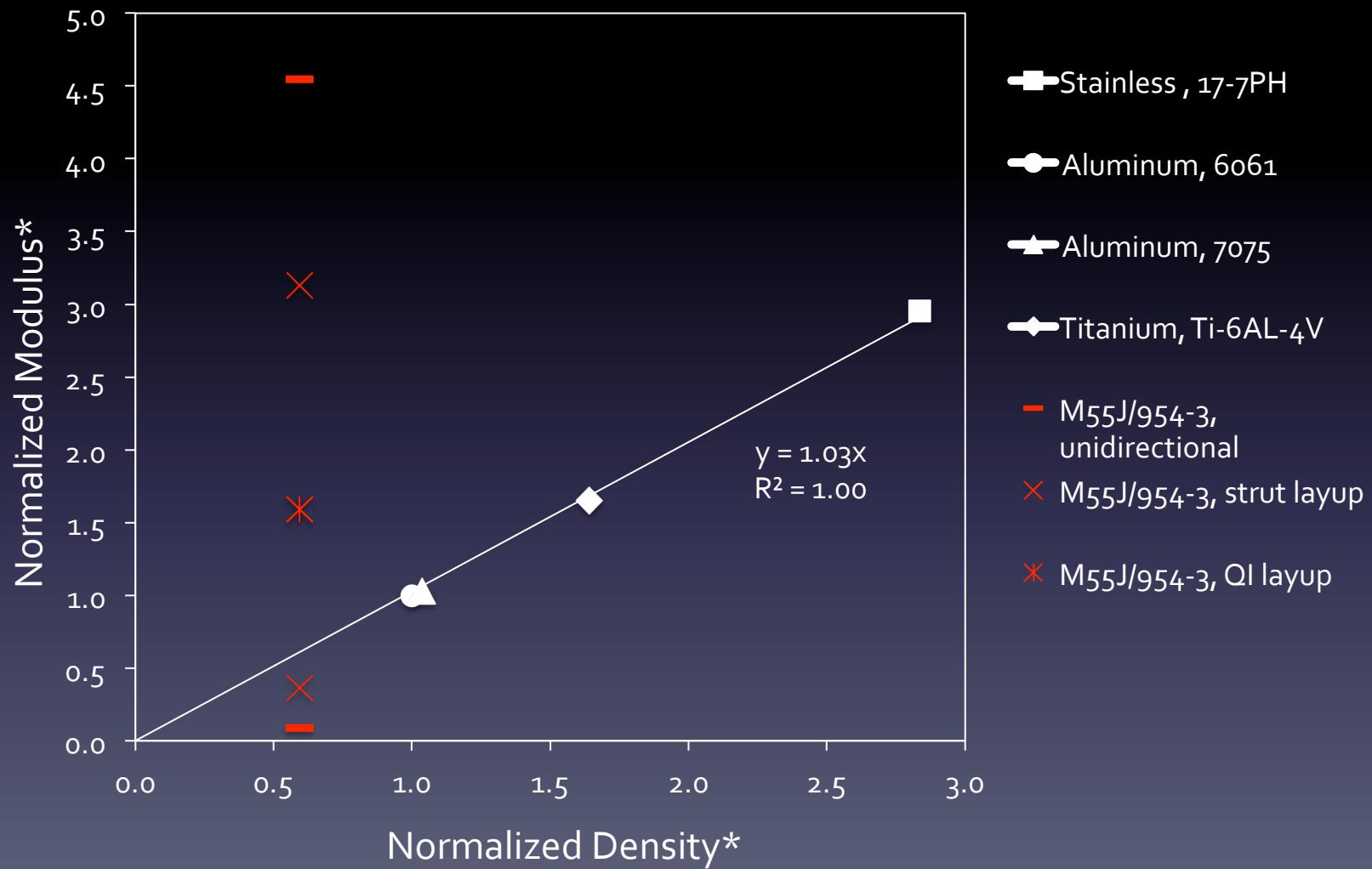
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Specific Stiffness

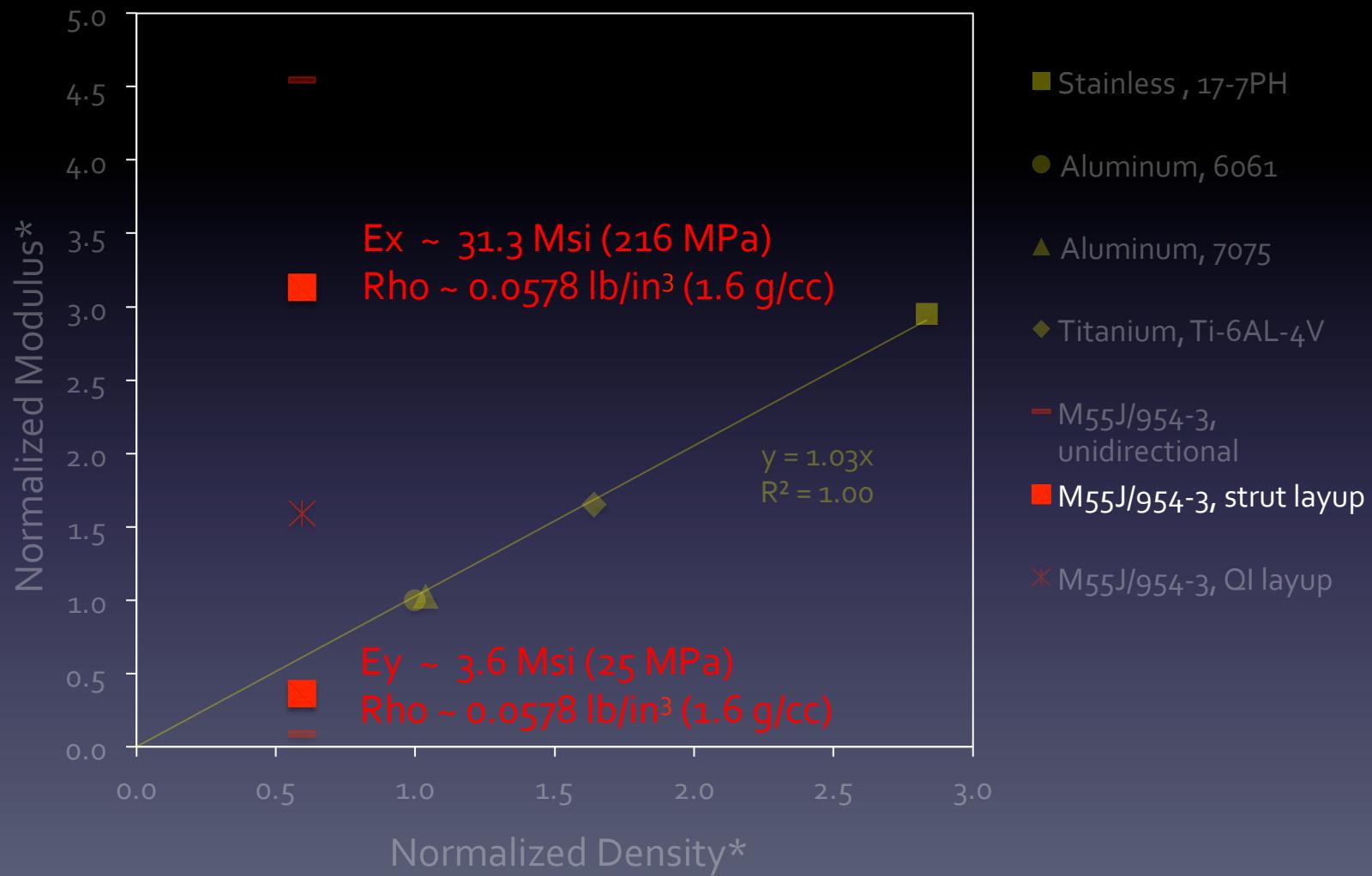
- As a preliminary metric, specific stiffness (modulus/density) is a good selection criteria for stiffness critical applications, such as struts and booms.
- For composites, one must carefully consider the type of loading, unidirectional vs omnidirectional, when evaluating design options, due to their anisotropic nature.

Specific Stiffness



*normalized by Aluminum 6061 properties

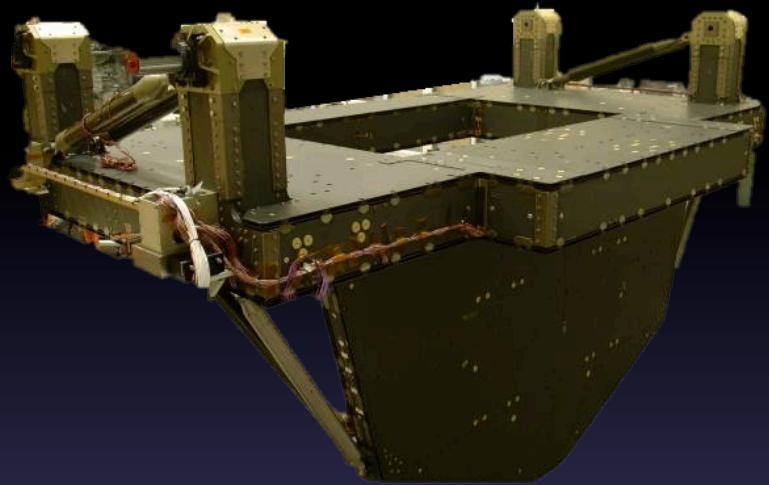
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Strut Application

SLIC Flight Structure



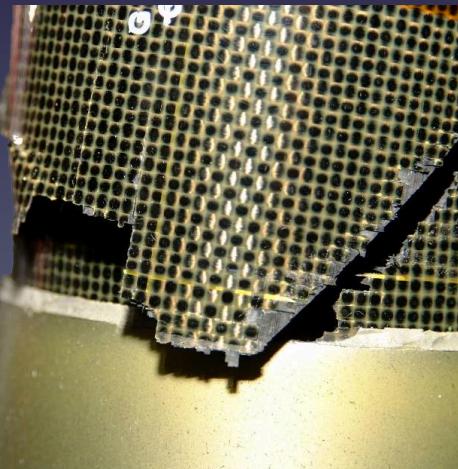
Development Testing



Tension Failure



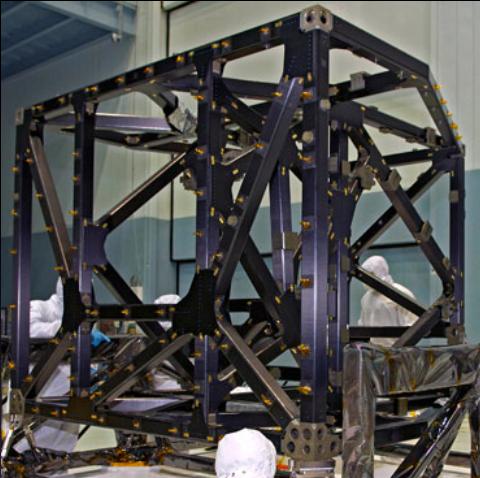
Compression Failure



- For strut application
 - Often required to limit deflections
 - E*A becomes a critical design constraint
- For equivalent E*A designs:
 - Composite = 0.06 lb/in (3 lb per 52 in)*
 - Metallic (Al or Ti-6-4) = 0.31 lb/in (16lb per 52 in)*

*does not account for end details

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Coefficient Of Thermal Expansion (CTE)

- For optical metering structures, a low thermal expansion coefficient is often required or eliminates the need for active thermal control
- Composite materials not only have low thermal expansion but it can be tailored based on the operational temperature needs of the observatory

Coefficient Of Thermal Expansion (CTE)

Composite truss tube (x-dir)

Silicon
Invar

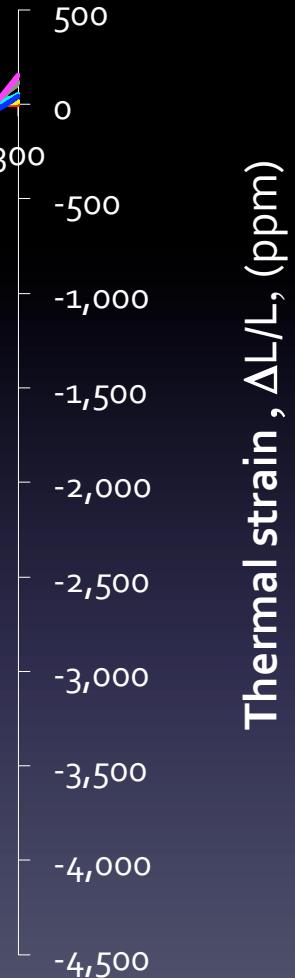
Ti-6Al-4V

G-10

SS 316

Al 6061-T6

Temperature (K)



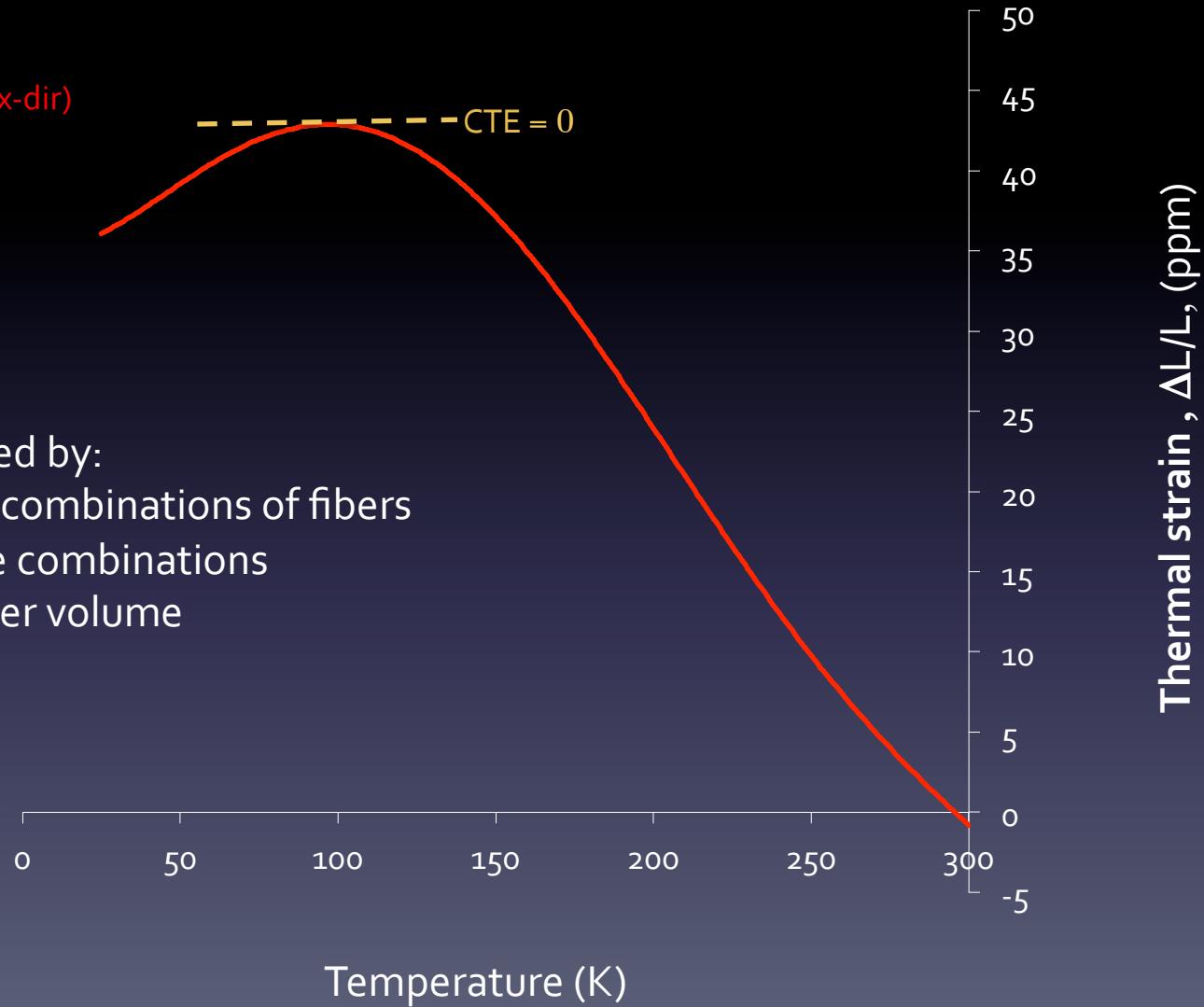
CTE = slope of $\Delta L/L$ vs T curve

Coefficient Of Thermal Expansion (CTE)

Composite truss tube (x-dir)

CTE can be tailored by:

- Using various combinations of fibers
- Tailoring angle combinations
- Controlling fiber volume



Recently Developed Composite Structures

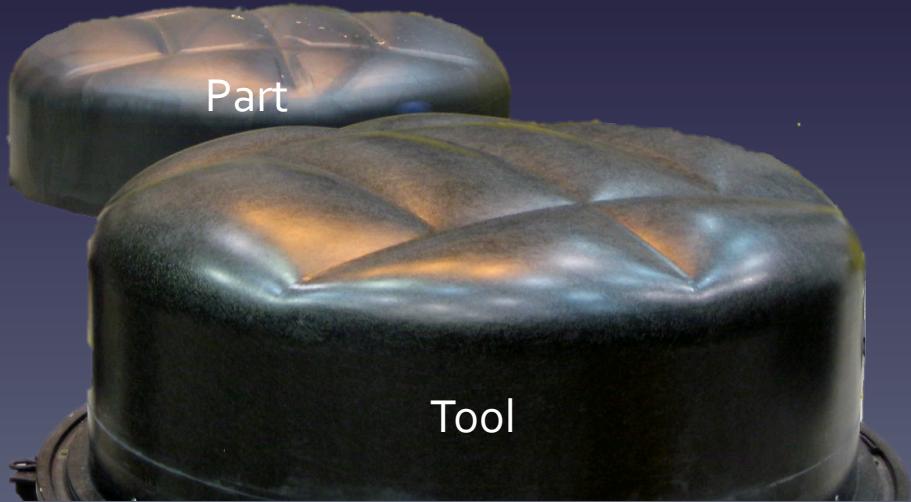
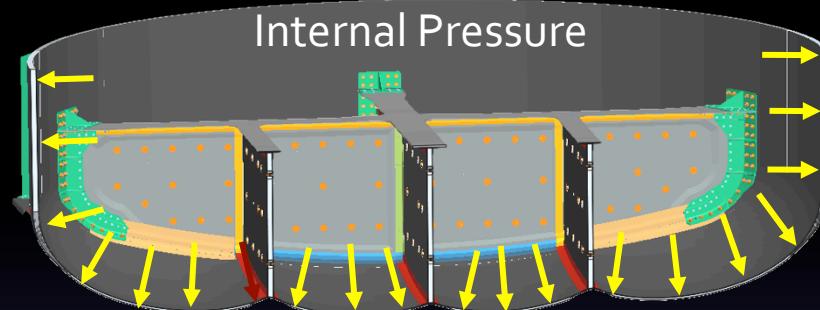
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Optimized Load Path

- Composites offer two unique properties that allow a designer to optimize the load path:
 - fiber orientation tailoring
 - forming complex contours easily/affordably

Optimized Load Path

- Backbone carries pressure load (no ring frame)
- Membrane pressure head lobe shapes

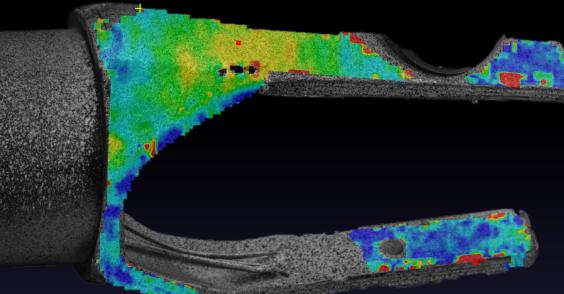
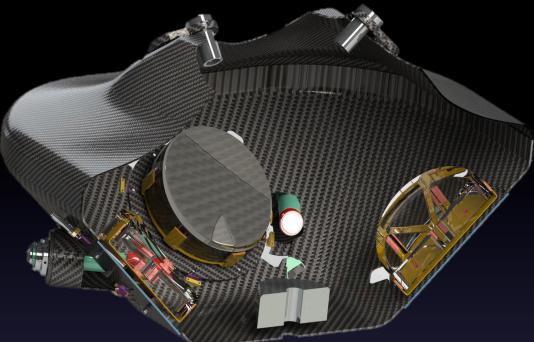


Other Primary Benefits of Composites for Spacecraft applications

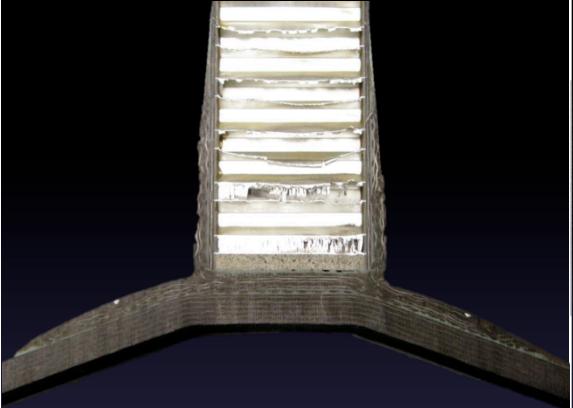
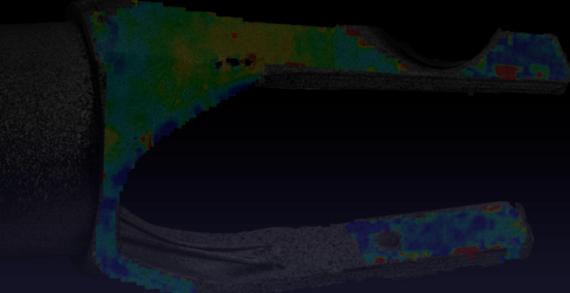
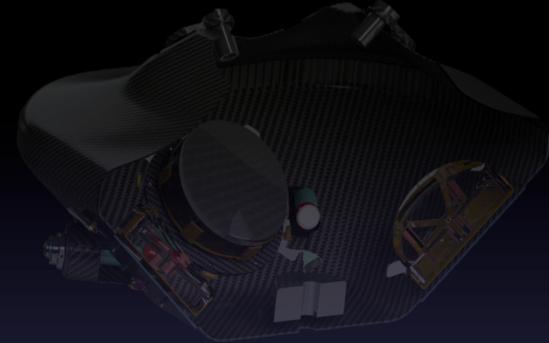
- Demisable for re-entry requirements
- Minimized interference for electromagnetic-sensitive instruments/applications
- High or low thermal (fiber dependent) conductivity along primary structural load paths for thermal management

COMPOSITE TECHNOLOGY THRUST AREAS FOR SPACE APPLICATIONS

Technology Thrust Areas

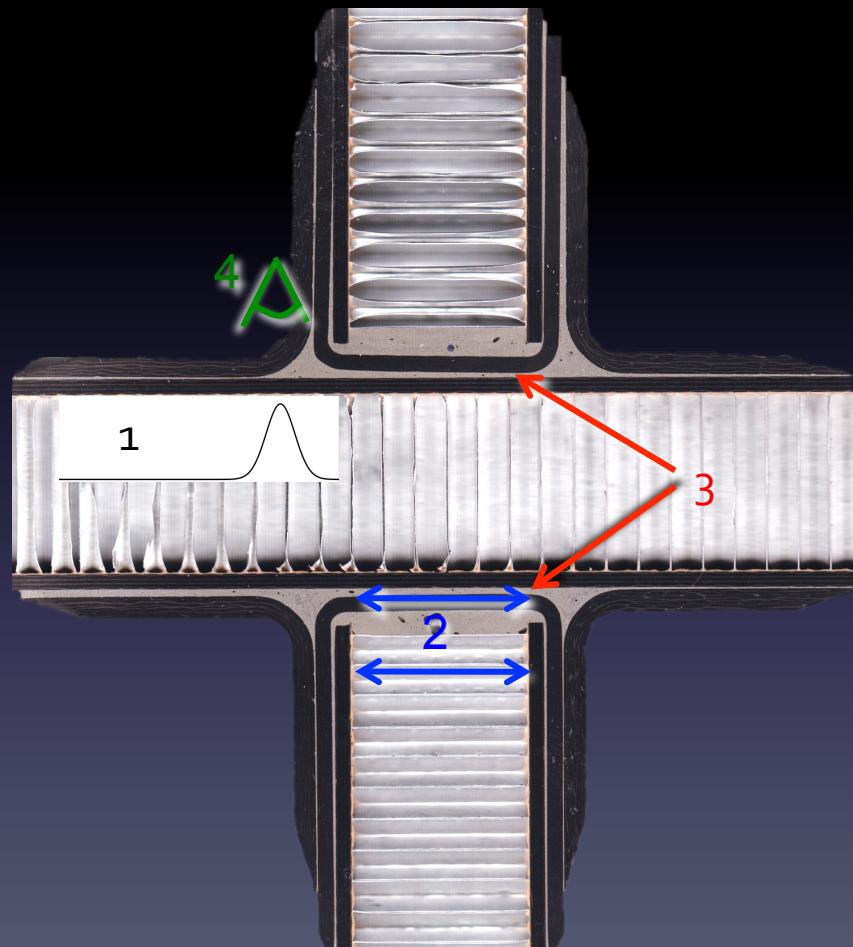
Thrust Area	Composite Joints	Development Cycle	Monocoque construction
Configuration			
Program	CCM and CoEx	GoCoMET	GSFC IRAD and GoCoMET
Composite benefit	<ul style="list-style-type: none"> • CTE matched joint • Mass savings • Performance enhancement 	<ul style="list-style-type: none"> • Reduction in “art-to-part” cycle time 	<ul style="list-style-type: none"> • Reduced part count • Optimized load path
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Technology Thrust Areas

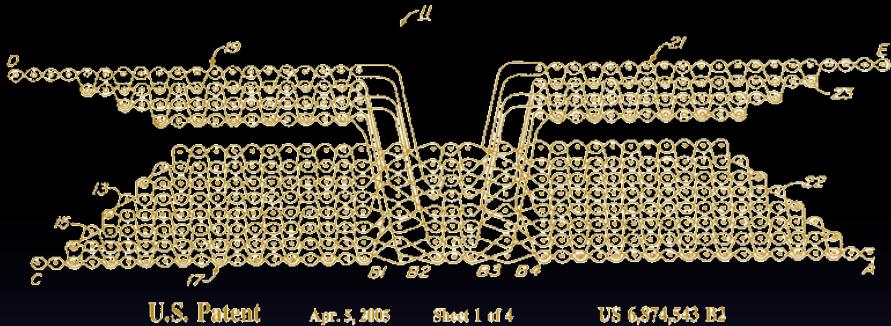
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Composite Joints: The Orthogonal Joint Challenge

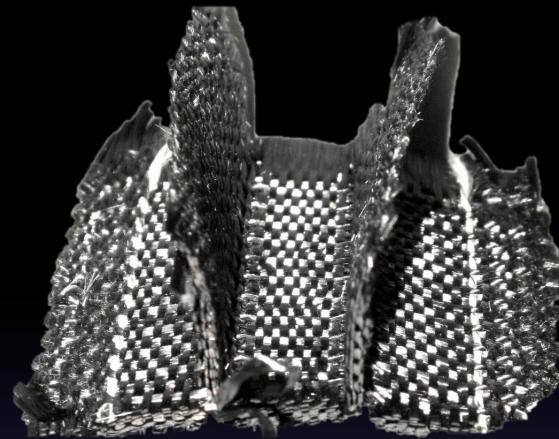
1. **Design Constraint:** This type of joint loads a composite laminate or sandwich in its weak direction (through-thickness tension).
2. **Analysis constraint:** This type of joint can introduce complex thermal stresses due to the orientation of the in-plane and through thickness orientations of the adjacent members.
3. **Manufacturing constraint:** Difficult to manage tolerance stack-up on large assemblies, leading to complex tooling for fully co-cured structures and/or bondline variability for pre-cured assembly.
4. **NDE constraint:** The weakest part of the joint is often not inspectable (location of peak stress at L-clip corner).



Composite Joints: 3D Woven Pi Preforms



Leveraged DoD funded and Lockheed Martin's patented 3D woven pi preform

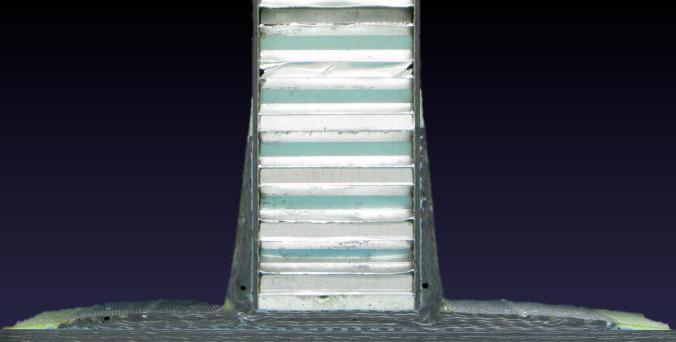


Hexcel IM7 High Strength Fiber
Bally Ribbon Mills Weave



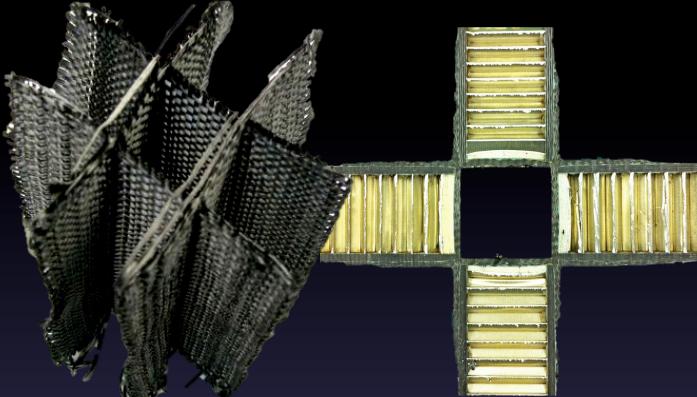
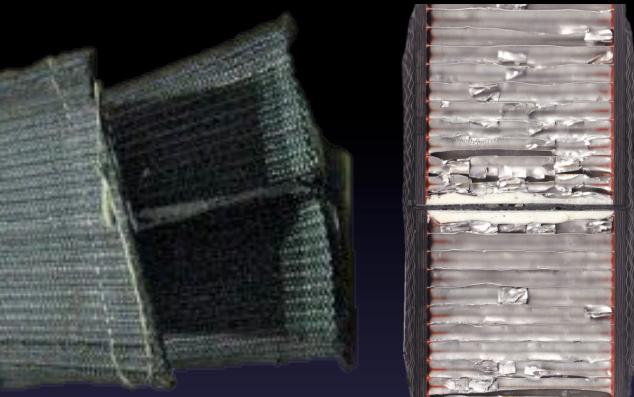
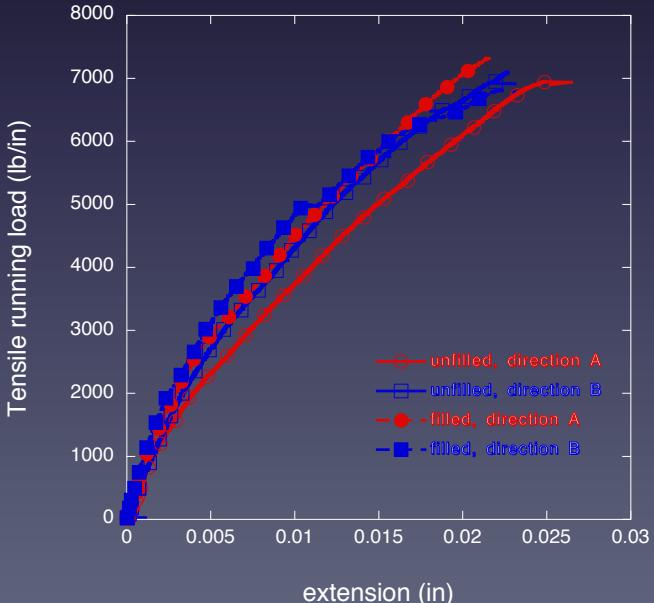
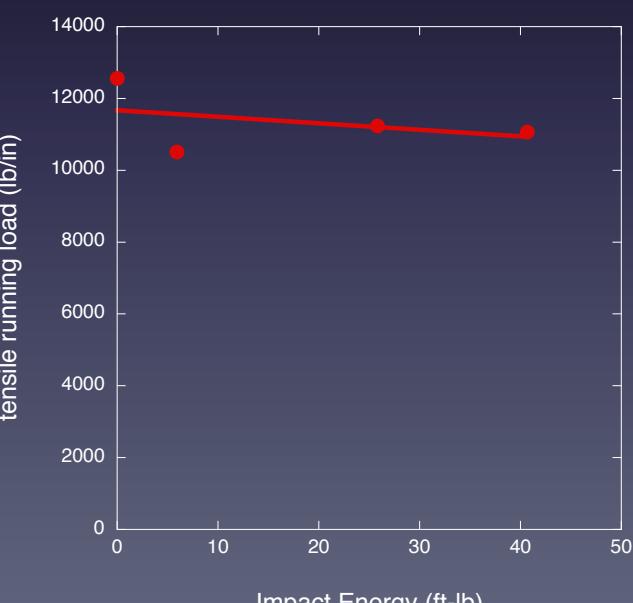
CCM Implementation on complex
contoured surface

Composite Joints: Performance Comparison

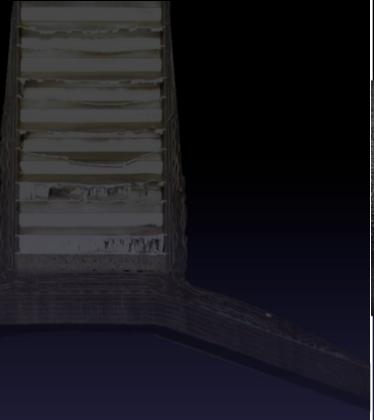
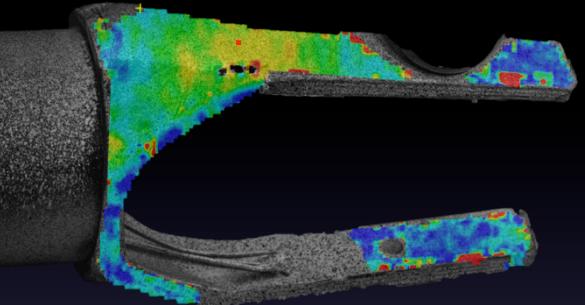
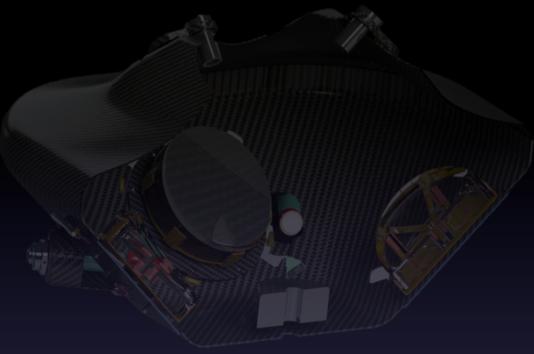
Program	HST's Super Lightweight Interchangeable Carrier	NESC's Composite Crew Module
Joint type	traditional back-to-back L-clips	3D woven pi preform
Geometry		
Pre-cured part count	5 pre-cured details: web, skin, closeout, two L-clips	2 pre-cured details: web and skin
Bonding process	2 step paste bond	1 step cobond
Tension Capability*	~900 lb/in	~2000 lb/in

*boundary condition dependent

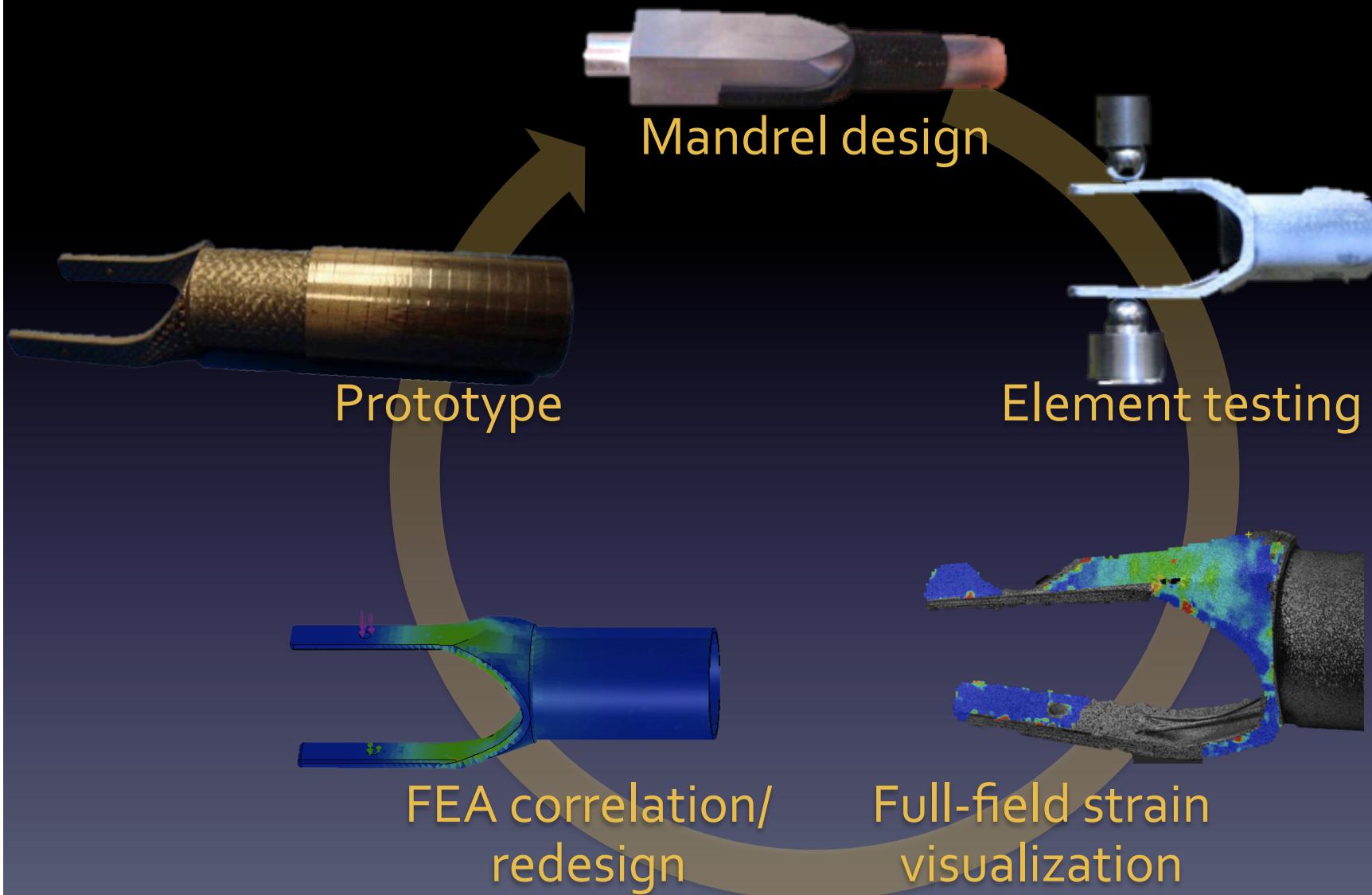
Composite Joints: Extending 3D Woven Capabilities

Program	NESC's Composite Crew Module	Composites for Exploration																																																			
Joint type	Cruciform	H-preform																																																			
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Performance	<p>Tensile running load (lb/in)</p>  <table border="1"> <caption>Estimated data points for Tensile running load vs extension</caption> <thead> <tr> <th>Extension (in)</th> <th>Unfilled, direction A (lb/in)</th> <th>Unfilled, direction B (lb/in)</th> <th>Filled, direction A (lb/in)</th> <th>Filled, direction B (lb/in)</th> </tr> </thead> <tbody> <tr><td>0.001</td><td>100</td><td>100</td><td>100</td><td>100</td></tr> <tr><td>0.002</td><td>200</td><td>200</td><td>200</td><td>200</td></tr> <tr><td>0.005</td><td>400</td><td>400</td><td>400</td><td>400</td></tr> <tr><td>0.01</td><td>800</td><td>800</td><td>800</td><td>800</td></tr> <tr><td>0.02</td><td>1600</td><td>1600</td><td>1600</td><td>1600</td></tr> <tr><td>0.025</td><td>2000</td><td>2000</td><td>2000</td><td>2000</td></tr> </tbody> </table> <p>extension (in)</p>	Extension (in)	Unfilled, direction A (lb/in)	Unfilled, direction B (lb/in)	Filled, direction A (lb/in)	Filled, direction B (lb/in)	0.001	100	100	100	100	0.002	200	200	200	200	0.005	400	400	400	400	0.01	800	800	800	800	0.02	1600	1600	1600	1600	0.025	2000	2000	2000	2000	<p>tensile running load (lb/in)</p>  <table border="1"> <caption>Estimated data points for Impact Energy vs tensile running load</caption> <thead> <tr> <th>Tensile Running Load (lb/in)</th> <th>Unfilled, direction A (ft-lb)</th> <th>Unfilled, direction B (ft-lb)</th> <th>Filled, direction A (ft-lb)</th> </tr> </thead> <tbody> <tr><td>12500</td><td>~5</td><td>-</td><td>-</td></tr> <tr><td>11500</td><td>-</td><td>~5</td><td>-</td></tr> <tr><td>10500</td><td>-</td><td>-</td><td>~5</td></tr> </tbody> </table> <p>Impact Energy (ft-lb)</p>	Tensile Running Load (lb/in)	Unfilled, direction A (ft-lb)	Unfilled, direction B (ft-lb)	Filled, direction A (ft-lb)	12500	~5	-	-	11500	-	~5	-	10500	-	-	~5
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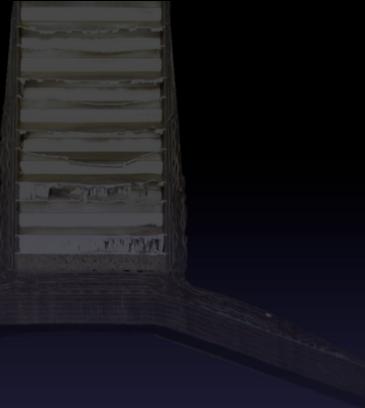
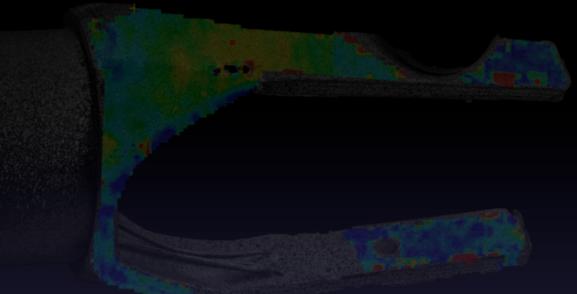
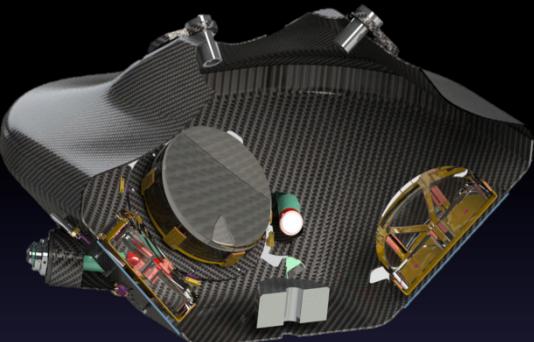
Technology Thrust Areas

Thrust Area	Composite Joints	Development Cycle	Monocoque construction
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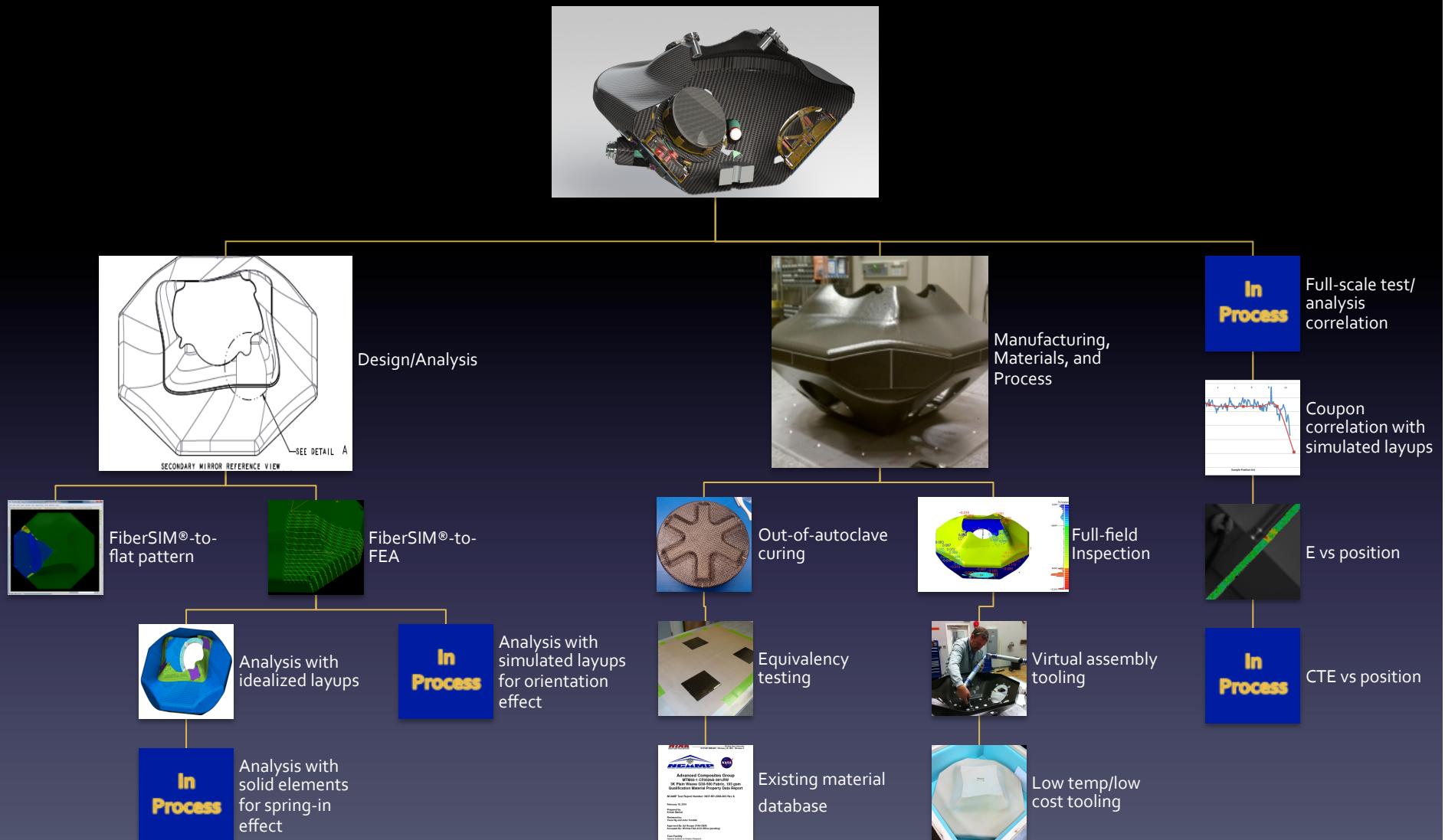
Rapid Prototyping: Reducing Development Cycle Time



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Monocoque Construction: Development Roadmap



Low volume production (1 or 2 units) requires minimization of fixed cost investments (tooling/fixturing)

Acknowledgements

GoCoMET	GSFC Materials Engineering	GSFC Advance Manufacturing	SLIC	ISIM	CCM	ACT
<ul style="list-style-type: none">•Michael Akkerman (OSC)•Terry Fan (GSFC)•Babak Farrokh (GSFC)•Ron Glenn (J&T)•Ben Rodini (SGT)•Ken Segal (GSFC)	<ul style="list-style-type: none">•Charles He (Ball)•Justin Jones (GSFC)•Bob Kiwak (Ball)•Brad Parker (GSFC)•Marc Russell (intern)•Mike Viens (GSFC)	<ul style="list-style-type: none">•Tony Baltusis (Bastion)•Kevin Compton (J&T)•Charles English (J&T)•Aleksey Luzhin (Bastion)•Harry Montgomery (J&T)•Seth Muse (Oceaneering)•Russell Rowles (J&T)	<ul style="list-style-type: none">•Marc Dinardo (LM)•Steve Hoyle (OSC)•Mike Oetkin (OSC)•FMW Composites•AASC	<ul style="list-style-type: none">•Wes Alexander (GSFC)•Jason Hylan (GSFC)•Eric Johnson (GSFC)•John Johnston (GSFC)•Carol Jones (GSFC)•Jim Pontius (GSFC)•ATK	<ul style="list-style-type: none">•Ian Fernandez (ARC)•Ken Hodges (GSFC)•Wade Jackson (LaRC)•Jim Jeans (SDA, Inc.)•Sotiris Kellas (LaRC)•Mike Kirsch (LaRC)•Larry Pelham (MSFC)•Ron Schmidt (LM)•Jeff Stewart (GSFC)•ATK•Bally Ribbon Mills	<ul style="list-style-type: none">•Ed Faust (SGT)•Pat Jordan (GSFC)•Dave Paddock (LaRC)•Chris Tolman (Genesis)

Questions?

Conscious

